

单管放大

共源

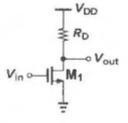
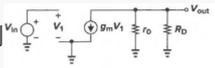
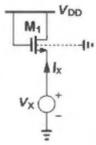
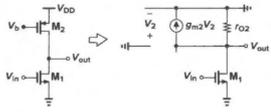
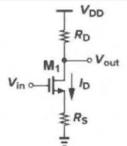
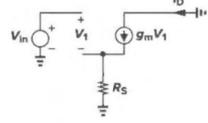
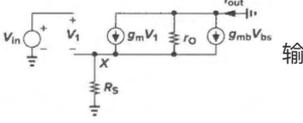
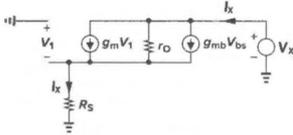
		共源放大	
电阻负载		$A_v = \frac{\partial V_{ow}}{\partial V_{in}}$ $= -R_D \mu_n C_{ox} \frac{W}{L} (V_{in} - V_{TH})$ $= -g_m R_D$	
考虑沟长调制		$A_v = -g_m (r_o \parallel R_D)$	
二极管负载		$\frac{V_x}{I_x} = \frac{1}{g_m + g_{mb} + r_n^{-1}}$ $= \frac{1}{g_m + g_{mb}} \parallel r_o$ $\approx \frac{1}{g_m + g_{mI}}$	
二极管负载增益		$A_v = -g_{m1} \frac{1}{g_{m2} + g_{mb2}}$ $= -\frac{g_{m1}}{g_{m2}} \frac{1}{1 + \eta}$ $= -\sqrt{\frac{(W/L)_1}{(W/L)_2}} \frac{1}{1 + \eta}$	
电流源负载		$A_v = -g_m (r_{O1} \parallel r_{O2})$	
带源极负反馈	 	$G_m = \frac{g_m}{1 + g_m R_s} = \frac{1}{\frac{1}{g_m} + R_s}$ <p style="text-align: right;">「在源极通路上看到的电阻」</p> $A_v = -G_m R_D$ $= \frac{-g_m R_D}{1 + g_m R_s}$	
考虑沟长调制与体效应:			

图 3.28

$$A_v = -\frac{R_D}{\frac{1}{g_{m1}} + \frac{1}{g_{m2}}}$$

出阻抗:



$$G_m = \frac{I_{out}}{V_{in}} = \frac{V_{out}}{V_{in}} \cdot \frac{I_{out}}{V_{out}}$$

$$= g_m r_o \cdot \frac{1}{R_{out}}$$

$$= \frac{g_m r_o}{r_o + [1 + (g_m + g_{mb})r_o]R_s} \rightarrow A_v = -G_m R_{out}$$

$$R_{out} = [1 + (g_m + g_{mb})R_s]r_o + R_s$$

$$= [1 + (g_m + g_{mb})r_b]R_s + r_o$$

带负载

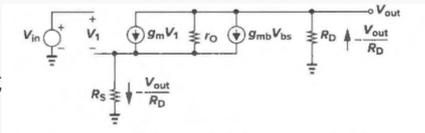


图 3.31 带有限的输出电阻的负反馈共源级的小信号等效电路

$$A_v = \frac{g_m r_o}{r_o + [1 + (g_m + g_{mb})r_o]R_s} (R_D // R_{out})$$

$$= \frac{g_m r_o}{R_s + r_o + (g_m + g_{mb})R_s r_o} \times \frac{R_D [R_s + r_o + (g_m + g_{mb})R_s r_o]}{R_D + R_s + r_o + (g_m + g_{mb})R_s r_o}$$

共漏

源跟随器 (共漏极)

忽略沟长调制

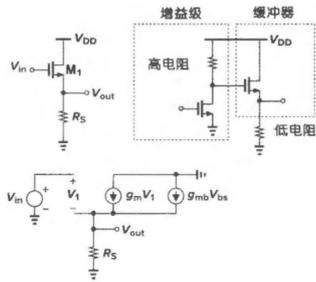


图 3.35 源跟随器的小信号等效电路

$$A_v = \frac{g_m R_s}{1 + (g_m + g_{mb})R_s} = \frac{R_s}{\frac{1}{g_m} + \left(\frac{g_m + g_{mb}}{g_m}\right)R_s}$$

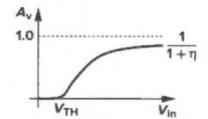
$$g_m = \mu_n C_{ox} \frac{W}{L} (V_m - V_{TH} - V_{ott})$$

小信号方法:

$$\begin{cases} V_{in} - V_1 = V_{out}, V_{bs} = -V_{out} \\ g_m V_1 - g_{mb} V_{out} = V_{out} / R_s \end{cases}$$

$$A_v = \frac{V_{out}}{V_{in}} = \frac{g_m R_s}{1 + (g_m + g_{mb})R_s}$$

$$A_v < 1$$



电流源代替电阻

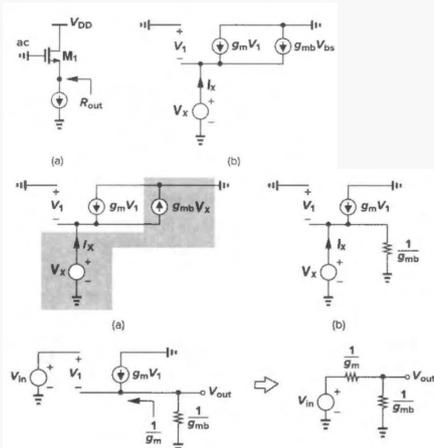


图 3.41 以戴维南等效表示本征源跟随器

$$R_{out} = \frac{1}{g_m} \parallel \frac{1}{g_{mb}} = \frac{1}{g_m + g_{mb}}$$

$$A_v = \frac{\frac{1}{g_{mb}}}{\frac{1}{g_m} + \frac{1}{g_{mb}}} = \frac{g_m}{g_m + g_{mb}}$$

驱动负载的源随器

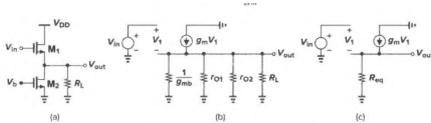


图 3.42 (a)驱动电阻负载的源跟随器;(b)小信号等效电路;(c)简化模式

$$A_v = \frac{R_{eq}}{R_{eq} + \frac{1}{g_m}}, R_{eq} = \left(\frac{1}{g_{mb}}\right) \parallel r_{o1} \parallel r_{o2} \parallel R_L$$

源随器不一定是有效的驱动器。

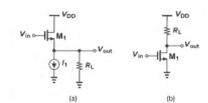
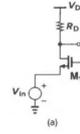
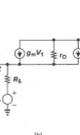
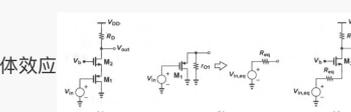
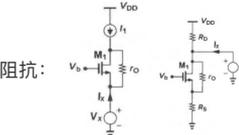
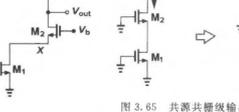
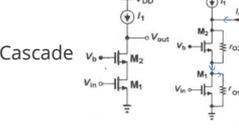
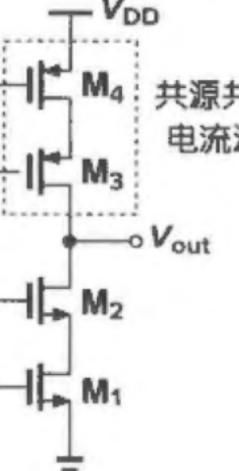


图 3.46 (a)源跟随器;(b)驱动电阻负载的共源级

共栅

<p>不考虑沟长调制</p> 	<p>共栅极</p> $\frac{\partial V_{out}}{\partial V_{in}} = \mu_n C_{ox} \frac{W}{L} R_D (V_b - V_{in} - V_{TH})(1 + \eta)$ $= g_m(1 + \eta)R_D$	<p>体效应使共栅级的等效跨导变大了</p>
<p>考虑MOS输出阻抗R_0及V_{in}阻抗R_s</p>  <p>图 3-51 (a) 输出电阻为有限值的共栅极 (b) 小信号等效电路</p>	$r_{ov} \left(\frac{-V_{out}}{R_D} - g_m V_1 - g_{mb} V_1 \right)$ <p>流过r_o电流</p> $- \frac{V_{out}}{R_D} R_S + V_{in} = V_{out}$ <p>and: $V_1 - \frac{V_{out}}{R_D} R_S + V_{in} = 0$</p> $\rightarrow: \frac{V_{out}}{V_{in}} = \frac{(g_m + g_{mb})r_o + 1}{r_o + (g_m + g_{mb})r_o R_S + R_S + R_D} R_D$	
<p>考虑沟长调制及体效应</p> 	<p>共源共栅级(cascade)</p> $V_{in,eq} = \frac{r_{o1} \parallel \frac{1}{g_{mb1}}}{r_{o1} \parallel \frac{1}{g_{mb1}} + \frac{1}{g_{m1}}} V_{in}, R_{eq} = r_{on} \parallel \frac{1}{g_{mb1}} \parallel \frac{1}{g_{m1}}$ <p>Replace it with: $\frac{V_{out}}{V_{in}}$</p>	
<p>共栅极输入输出阻抗:</p> 	$R_x = \frac{V_x}{I_x} = \frac{r_o}{1 + (g_m + g_{mb})r_o}$ $= \frac{1}{\frac{1}{r_o} + g_m + g_{mb}}$ $= r_o \parallel \frac{1}{g_m} \parallel \frac{1}{g_{mb}}$ <p>理想电流源负载的共栅极输入电阻</p> $R_{out} = \{ [1 + (g_m + g_{mb})r_o] R_S + r_o \} \parallel R_D$ <p>带源级负反馈共栅极的输出电阻</p>	
<p>输出电阻:</p>  <p>图 3-59 共源共栅结构 图 3-65 共源共栅级输出电阻的计算</p>	$R_{out} = [1 + (g_{m2} + g_{mb2})r_{o2}]r_{o1} + r_{o2}$ $\approx (g_{m2} + g_{mb2}) \cdot r_{o1}r_{o2}$ <p>「共源共栅输出阻抗」</p>	
<p>带电流源负载的Cascade</p> 	$R_x = r_o \parallel \frac{1}{g_m} \parallel \frac{1}{g_{mb}}$ <p>M_1漏端看进去的负载</p> $I_{out} = g_{m1} V_{in} \frac{r_{o1}}{r_{o1} + r_o \parallel \frac{1}{g_m} \parallel \frac{1}{g_{mb}}}$ $G_m = \frac{I_{out}}{V_{in}} = \frac{g_{m1} r_{o1} [r_{o2} (g_{m2} + g_{mb2}) + 1]}{r_{o1} r_{o2} (g_{m2} + g_{mb2}) + r_{o1} + r_{o2}}$ $ A_v = G_m R_{out} = g_{m1} r_{o1} [r_{o2} (g_{m2} + g_{mb2}) + 1]$	<p>if $G_m \approx g_m$ then $A_v = g_{m1} R_{out}$</p>
<p>上图电流源用PMOS Cascade实现:</p> 	$R_{out} = \{ [1 + (g_{m2} + g_{mb2})r_{o2}]r_{o1} + r_{o2} \} \parallel \{ [1 + (g_{m3} + g_{mb3})r_{o3}]r_{o4} + r_{o3} \}$ $ A_v \approx g_{m1} [(g_{m2} r_{n2} r_{m1}) \parallel (g_{m3} r_{o3} r_{m3})]$	